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# Detecting information flow direction in multivariate linear and nonlinear models

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**ABSTRACT:** In this paper we present an approach to analyze the direction of information flow between time series involving bidirectional relations. The intuitive idea comes from a first study dedicated to the so-called phase slope index, which is a measure originally developed to detect unidirectional relations and is based on the complex coherence function. In order to detect bidirectional flows, we propose two new causality indices supplying the previous index with two other functions, the directed coherence function and the directed transfer function. Moreover, to cope with the inability of the approaches based on coherence (ordinary or directed) or on directed transfer function to distinguish between direct and indirect relations, we propose another causality index based on the partial directed coherence to identify only direct relations. Experimental results show that some challenges have promising solutions through the use of this new indicator dealing with both linear and nonlinear multivariate models.

**Keywords:** Effective connectivity; causal relations; partial directed coherence; information flow; multivariate time series.

## 1. Introduction

In neuroscience, investigating activated cortical networks, in particular detecting direct interactions (directional anatomical links physiologically activated) between different cortical sites, helps in understanding brain functioning. Over the last decade, a number of measures have been considered to deal with causal dependency in multiple areas, such as physics, economics, chaotic systems and more particularly, effective connectivity in neurophysiology [2, 5, 8, 12, 14-18]. Recently, a Phase Slope Index (PSI) was proposed by Nolte [11] to detect information flow in unidirectional propagation graphs. The idea behind this measure is that the slope of the cross-spectrum phase between two different source activities depends on the time needed for the information flow between those areas and on the corresponding direction. This method, based on the linear phase between two signals, estimates the direction by computing the slope of the phase of the ordinary coherence

function. Now, when two time series may display direct or indirect relations, PSI based on the ordinary coherence function fails to distinguish between these two types of relations. As a matter of fact, when a third channel accounts for the linear relation between two other signals under scrutiny, the amplitude of the coherence function between these two signals is one (as it is when there is a direct linear relation between these signals). To deal with this issue, we recently proposed to replace ordinary coherence with partial coherence [20]. As a matter of fact, let us consider the following simple scenario where signals  $x_1(t)$ ,  $x_2(t)$  and  $x_3(t)$  are given by:

$$\begin{cases} x_1(t) = 0.9x_1(t-1) + w_1(t) \\ x_2(t) = -0.5x_1(t-1) + w_2(t) \\ x_3(t) = 0.8x_2(t-2) - \alpha x_1(t-2) + w_3(t) \end{cases} \quad (1)$$

where  $w_i(t)$  ( $i=1,2,3$ ) are white Gaussian noises and the parameter  $\alpha$  is introduced so as to possibly consider indirect ( $\alpha=0$ ) or direct ( $\alpha=0.7$ ) relations between the two time series  $x_1(t)$  and  $x_3(t)$ . In this example, if we compute the PSI based on the ordinary coherence [11], we find comparable values whatever  $\alpha$  (for  $\alpha=0$ ,  $PSI=1.35$ , and for  $\alpha=0.7$ ,  $PSI=1.33$ ), whereas results are very different when PSI is computed from the partial coherence (for  $\alpha=0$ ,  $PSI=0.01$  whereas for  $\alpha=0.7$ ,  $PSI=0.95$ ) which concludes to the success of the second indicator in detecting direct relations. However, just like ordinary coherence, since the partial coherence function between two signals only carries a single direction's information (given by the phase itself and its opposite value), it leads to a symmetric indicator and, consequently, is unable to detect bidirectional flows. As a matter of fact, if we consider a second scenario operating on the following three signals:

$$\begin{cases} x_1(t) = 0.9x_1(t-1) + w_1(t) \\ x_2(t) = -0.5x_1(t-1) - 0.6x_3(t-2) + w_2(t) \\ x_3(t) = 0.8x_2(t-2) + w_3(t) \end{cases} \quad (2)$$

In this example, a bidirectional relation exists between the two time series  $x_2(t)$  and  $x_3(t)$ . Computing the PSI from  $x_2(t)$  to  $x_3(t)$  using coherence (resp. partial coherence) leads to a value close to 1.7 (resp. 0.7) whereas the PSI from  $x_3(t)$  to  $x_2(t)$  returns the opposite value, *i.e.* -1.7 (resp. -0.7), so that it becomes impossible to detect bidirectional flows. So, the aim of the present work is to mitigate the two previous issues. On the one hand, we investigate new causality indices (CI) to detect and differentiate unidirectional and bidirectional relations between multivariate time series (Fig. 1(a) and 1(b)): the first one is a new CI based on the directed coherence (DCOH) function [13] when considering pairwise analysis (*i.e.* only two observations are considered at the same time) and the second one is based on the directed transfer function (DTF) [9, 20] when considering multivariate analysis (*i.e.* joint analysis of more than two signals). On the other hand, to meet potential direct and indirect relations in bidirectional situations (Fig. 1(a) and 1(c)), we recommend to introduce partial directed coherence (PDC) [3] in a new indicator. Until now, only the amplitudes of these different transfer functions have been consid-

ered in the literature to estimate the so-called functional connectivity between structures in the frequency domain. Such approaches obviously failed in differentiating even quite simple scenarios, e.g. when two investigated observations only consisted of different time shifted versions of a third observation. In this paper, the three proposed causality indices are detailed theoretically in the next section. Linear and nonlinear time series are considered in a third section to test these indices and compare their performance before drawing some conclusions.

## 2. Methods and materials

Phase slope index (PSI) is a method to evaluate unidirectional information flows in pairs of signals [11]. After reviewing its concept and pointing out its theoretical limitations, we develop three new causality indices respectively based on DCOH, DTF and PDC.

### 2.1. Phase slope index

The PSI basic hypothesis relies on the exploitation of the phase monotony between signals which appears when the frequency components of one signal precede temporally those of another signal [11]. PSI is defined in order to summarize information on the slope of the phase of the cross-spectrum between two time series  $x_m(t)$  and  $x_n(t)$ ,  $t = 1, 2, \dots, T$ , where  $T$  is the signal length. The theoretical idea of this index is to properly represent relative time delays between spectral components of the two signals  $x_m$  and  $x_n$  only in the frequency bands leading to a significant value of the coherence function. To justify the formula introduced by Nolte to define his index, we consider the functional

$$\nabla_{m,n} = \int \frac{\partial \theta(f)}{\partial f} |C_{mn}(f)|^2 df \quad (3)$$

where  $C_{mn}(f) = S_{mn}(f) / \sqrt{S_{mm}(f)S_{nn}(f)}$  is the ordinary coherence function between signals  $x_m$  and  $x_n$ , with  $C_{mn}(f) = |C_{mn}(f)| \exp(i\theta(f))$  and where the phase slope  $\frac{\partial \theta(f)}{\partial f}$ , when it is constant, corresponds to a pure delay. Clearly, the squared magnitude of the coherence,  $|C_{mn}(f)|^2$ , provides weighting the phase slope and, consequently, decreases its impact when it is low. Hence, this functional is sensitive to both phase slope and coherence magnitude. As explained below the following expression

$$\text{Im} \left( \sum_{f \in F_d} C_{mn}^*(f) C_{mn}(f + \delta_f) \right) \quad (4)$$

is a numerical approximation of  $\nabla_{m,n}$  which corresponds to the Phase slope index defined in [11] and is noted  $\text{PSI}_{mn}$ .

$\text{Im}(\bullet)$  denotes the imaginary part and the asterisk, the conjugate value;  $F_d$  is a discrete set of frequencies over which the index is computed and which can be chosen by the experimenter according to some knowledge on the signals' characteristics. For example, if it is known that the signals are band limited,  $F_d$  can be reduced to only some critical frequencies. Similarly, when using FFT and without any a priori knowledge on the signals, the maximum set in the normalized half frequency band

is given by:  $F_d = \{0, 1/N, \dots, 1/2 - \delta_f\}$  where  $\delta_f = 1/N$  (in this case the frequential step-size  $\delta_f$  corresponds to the frequency resolution  $1/N$ ). The auto-spectral density functions  $S_{mm}(f)$  and  $S_{nn}(f)$  are the Fourier transforms of the auto-correlation of the signals  $x_m(t)$  and  $x_n(t)$  respectively, the cross-spectral density function  $S_{mn}(f)$  is the Fourier transform of the cross-correlation between signals  $x_m(t)$  and  $x_n(t)$  defined by  $E[x_m(t)x_n^*(t-\tau)]$ , where  $E[\bullet]$  is the expectation operator and  $\tau$  is a time displacement. With  $C_{mn}(f) = |C_{mn}(f)|\exp(i\theta(f))$ , we can write  $PSI_{mn} = \sum_{f \in F} \sin(\theta(f + \delta_f) - \theta(f)) |C_{mn}(f)C_{mn}(f + \delta_f)|$ , which can be approximated, for a sufficiently small  $\delta_f$ , by  $PSI_{mn} \approx \sum_{f_i \in F_d} (\theta(f_i + \delta_f) - \theta(f_i)) |C_{mn}(f_i)|^2 \approx \int_{f \in F} \frac{\partial \theta(f)}{\partial f} |C_{mn}(f)|^2 df$  where the second term corresponds to a Riemann sum which is based on the assumption that the frequencies in  $F_d$  are regularly spaced with  $\delta_f$  spacing and approximates the continuous sum (third term) on a continuous range  $F$ . The sign of PSI indicates the flow direction and its magnitude increases along with the delay and the coherence module. Clearly, this index (i) only works in situations of unidirectional connections, and (ii) cannot discriminate between direct and indirect relations. Following our notations, a positive value of  $PSI_{mn}$  means that the signal  $x_n$  is a delayed version of  $x_m$ . As it is well known, the linearity of the phase corresponds to a pure delay between signals  $x_m$  and  $x_n$ . When one signal contributes to the second with multiple, different delays, the phase becomes nonlinear (the slope is no longer a constant). Nevertheless, to deal with a more general situation, we extend this idea to other coupling based functions as the phase is monotonic to propose novel causality indices, noted CI hereafter. While ordinary coherence focuses on mutual interaction of the structures themselves, directed coherence as well as directed transfer function refer more to the concept of Granger causality. This concept stipulates that a time series  $x_i(t)$  causes another series  $x_j(t)$  if the knowledge of  $x_i(t)$ 's past significantly improves the prediction of  $x_j(t)$ . In this sense, only past samples are considered in improving prediction. Consequently, unlike ordinary coherence, directed coherence and directed transfer function are asymmetric quantities.

## 2.2. Causality index using directed coherence

The concept of directed coherence was first developed by Saito and Harashima [13] to jointly analyze information production in two time series, each having its proper white noise source, which can be seen as a local innovation, as well as a common source, seen as an external innovation. This can be represented with a bivariate autoregressive (AR) model for the production of signals. While coherence measures the degree of linear correlation as a total, the "directed coherences" can be seen as "correlations with direction" between the two observed signals expressed in the frequency domain and, interestingly, be regarded as two contributing weighted factors in the expression of the global coherence. Given these two observations (outputs of the system), these coherences describe the connection between the first (resp. second) noise input and the second

(resp. first) output of the system.

To formulate this problem of direction of correlating influences, Saito and Harashima considered a bivariate autoregressive process of order  $p$  including a common noise source  $w_3(t)$  as follows:

$$\begin{pmatrix} x_1(t) \\ x_2(t) \end{pmatrix} = \sum_{k=1}^p \begin{pmatrix} \alpha_{11}(k) & \alpha_{12}(k) \\ \alpha_{21}(k) & \alpha_{22}(k) \end{pmatrix} \begin{pmatrix} x_1(t-k) \\ x_2(t-k) \end{pmatrix} + \begin{pmatrix} b_{11} & b_{13} & 0 \\ 0 & b_{23} & b_{22} \end{pmatrix} \begin{pmatrix} w_1(t) \\ w_3(t) \\ w_2(t) \end{pmatrix} \quad (5)$$

where variables  $b_{mn}$ ,  $m \in \{1,2\}$ ,  $n \in \{1,2,3\}$ , are weight factors,  $w_j(t)$ ,  $j=1,2,3$  are independent zero mean white

Gaussian noises of unit variance. In the frequency domain, we have the spectral equivalent model:

$$\begin{aligned} \begin{pmatrix} dX_1(f) \\ dX_2(f) \end{pmatrix} &= \begin{pmatrix} 1 - \sum_{k=1}^p \alpha_{11}(k) e^{-2i\pi fk} & -\sum_{k=1}^p \alpha_{12}(k) e^{-2i\pi fk} \\ -\sum_{k=1}^p \alpha_{21}(k) e^{-2i\pi fk} & 1 - \sum_{k=1}^p \alpha_{22}(k) e^{-2i\pi fk} \end{pmatrix}^{-1} \begin{pmatrix} b_{11} & b_{13} & 0 \\ 0 & b_{23} & b_{22} \end{pmatrix} \begin{pmatrix} dW_1(f) \\ dW_3(f) \\ dW_2(f) \end{pmatrix} \\ &= \begin{pmatrix} A_{11}(f) & A_{12}(f) \\ A_{21}(f) & A_{22}(f) \end{pmatrix} \begin{pmatrix} b_{11} & b_{13} & 0 \\ 0 & b_{23} & b_{22} \end{pmatrix} \begin{pmatrix} dW_1(f) \\ dW_3(f) \\ dW_2(f) \end{pmatrix} \end{aligned} \quad (6)$$

where  $dX_1(f)$  and  $dX_2(f)$  are the infinitesimal random spectral components [4] of the second order stochastic signals  $x_1(t)$  and  $x_2(t)$ ,  $dW_j(f)$  are those of the input noises  $w_j(t)$ ,  $j=1,2,3$ . Then, we introduce the matrix  $H(f)$  such as:

$$H(f) = \begin{pmatrix} H_{11}(f) & H_{13}(f) & H_{12}(f) \\ H_{21}(f) & H_{23}(f) & H_{22}(f) \end{pmatrix} = \begin{pmatrix} A_{11}(f) & A_{12}(f) \\ A_{21}(f) & A_{22}(f) \end{pmatrix} \begin{pmatrix} b_{11} & b_{13} & 0 \\ 0 & b_{23} & b_{22} \end{pmatrix}. \quad (7)$$

The DCOH estimate of the linear feedback from the innovation process  $w_m(t)$  corresponding to the observation  $x_m(t)$  to the observed signal  $x_n(t)$ , with  $m \neq n \in \{1,2\}$ , is

$$DCOH_{mn}(f) \triangleq \frac{H_{nm}(f)}{\sqrt{\sum_{j=1,2,3} |H_{nj}(f)|^2}}. \quad (8)$$

Following the previous idea on PSI, we defined a causality index, named CI-DCOH, as follows:

$$CI_{mn}\text{-DCOH} = \text{Im} \left( \sum_{f \in F} DCOH_{mn}^*(f) DCOH_{mn}(f + \delta_f) \right). \quad (9)$$

Contrary to the PSI, this index is asymmetric allowing the detection of bidirectional flows. It is no longer relative to the slope of the phase between the observations themselves but to those between the noise sources  $w_m(t)$  and the signals  $x_n(t)$ , with  $m \neq n \in \{1,2\}$ .

### 2.3. Causality index using directed transfer function

Following the concept of directed coherence, the directed transfer function (DTF) was introduced by Kamiński and Blińska [9] to deal with a number of observations greater than two. In this case, contrary to the previous situation, no hidden common noise source is considered, and each observation can be viewed as produced by its own innovation sequence linearly combined with delayed versions of all observations. In the same manner as previously, directed transfer function from the  $i$ -th input to the  $j$ -th output of the system can be derived. Let it be indicated that both estimators are normalized with

respect to the structure that receives the signal. So, in the framework of multivariate observations, we extend the aforementioned concept of causality index to DTF (instead of DCOH). Let  $x_1, x_2, \dots, x_Q$  be  $Q$  zero mean signals whose discrete-time observations are noted  $x_1(t), x_2(t), \dots, x_Q(t)$ . Suppose a multivariate AR model of order  $p$  to represent the observations. Using the lag operator  $L$  ( $Lx_m(t) = x_m(t-1)$ ,  $m = 1, 2, \dots, Q$ ), we write

$$\underbrace{\begin{pmatrix} 1 - \sum_{k=1}^p \alpha_{11}(k)L^k & -\sum_{k=1}^p \alpha_{12}(k)L^k & \cdots & -\sum_{k=1}^p \alpha_{1Q}(k)L^k \\ -\sum_{k=1}^p \alpha_{21}(k)L^k & 1 - \sum_{k=1}^p \alpha_{22}(k)L^k & \cdots & -\sum_{k=1}^p \alpha_{2Q}(k)L^k \\ \vdots & \vdots & \ddots & \vdots \\ -\sum_{k=1}^p \alpha_{Q1}(k)L^k & -\sum_{k=1}^p \alpha_{Q2}(k)L^k & \cdots & 1 - \sum_{k=1}^p \alpha_{QQ}(k)L^k \end{pmatrix}}_{\alpha} \begin{pmatrix} x_1(t) \\ \vdots \\ x_Q(t) \end{pmatrix} = \begin{pmatrix} w_1(t) \\ \vdots \\ w_Q(t) \end{pmatrix}. \quad (10)$$

where  $w_m(t)$  are white Gaussian noises (innovations), and each regressor  $\alpha_{mn}(k)$ ,  $m, n \in \{1, 2, \dots, Q\}$ , evaluates the linear interaction of  $x_n(t-k)$  on  $w_m(t)$ . Applying Fourier transform to the transfer functions matrix  $\alpha$  in (10), we get the corresponding matrix  $D(f)$ :

$$D(f) = \begin{pmatrix} D_{11}(f) & D_{12}(f) & \cdots & D_{1Q}(f) \\ D_{21}(f) & D_{22}(f) & \cdots & D_{2Q}(f) \\ \vdots & \vdots & \ddots & \vdots \\ D_{Q1}(f) & D_{Q2}(f) & \cdots & D_{QQ}(f) \end{pmatrix} \quad (11)$$

where the components of the matrix  $D(f)$  are  $D_{mn}(f) = \begin{cases} 1 - \sum_{k=1}^p \alpha_{mn}(k)e^{-2i\pi fk}, & m = n \\ -\sum_{k=1}^p \alpha_{mn}(k)e^{-2i\pi fk}, & m \neq n \end{cases}$ .

Defining the transfer matrix  $H(f)$  as the inverse of the matrix  $D(f)$ , we obtain

$$H(f) = \begin{pmatrix} H_{11}(f) & H_{12}(f) & \cdots & H_{1Q}(f) \\ H_{21}(f) & H_{22}(f) & \cdots & H_{2Q}(f) \\ \vdots & \vdots & \ddots & \vdots \\ H_{Q1}(f) & H_{Q2}(f) & \cdots & H_{QQ}(f) \end{pmatrix} = \begin{pmatrix} D_{11}(f) & D_{12}(f) & \cdots & D_{1Q}(f) \\ D_{21}(f) & D_{22}(f) & \cdots & D_{2Q}(f) \\ \vdots & \vdots & \ddots & \vdots \\ D_{Q1}(f) & D_{Q2}(f) & \cdots & D_{QQ}(f) \end{pmatrix}^{-1}. \quad (12)$$

The Directed Transfer Function from channel  $m$  to channel  $n$  is defined by:

$$DTF_{mn}(f) \triangleq \frac{H_{nm}(f)}{\sqrt{\sum_{m=1}^Q |H_{nm}(f)|^2}} \quad (13)$$

where  $H_{nm}(f)$  is the  $(n, m)$  element of the matrix  $H(f)$ , corresponding to a normalized contribution of the input sequence  $w_m(t)$  onto the output signal  $x_n(t)$ . In the same way as before, we defined a causality index based on DTF, noted CI-DTF, as follows:

$$CI_{mn}\text{-DTF} = \text{Im} \left( \sum_{f \in F} DTF_{mn}^*(f) DTF_{mn}(f + \delta_f) \right). \quad (14)$$

#### 2.4. Causality index using partial directed coherence

Following the above developments, in [3] Baccalá and Sameshima contrasted partial directed coherence with directed coherence to show how partial directed coherence provides direct structural information for multivariate time signals, as partial coherence does compared to ordinary coherence in unidirectional flow models. So, given  $Q > 2$  observations, the partial directed coherence function describes the interaction between two of these observations when the influence due to all other  $Q - 2$  time series is discounted. According to Eq. (11), the PDC from  $x_m$  to  $x_n$  conditionally to other  $Q - 2$  signals can be written

$$PDC_{mn}(f) \triangleq \frac{D_{nm}(f)}{\sqrt{d_m^\dagger(f) \cdot d_m(f)}} \quad (15)$$

where  $D_{nm}(f)$  is the  $(n, m)$  element of  $D(f)$  and  $d_m(f)$  is the  $m$ th column of  $D(f)$ .  $D_{nm}(f)$  represents the part of the past of  $x_m$  on the present signal  $x_n$ . The sign  $\dagger$  denotes conjugate transpose. The arguments to define a PDC based causality index can be fully justified as we want to develop an average measure (i) to quantify the relative delays between multiple signals and not only to qualify them as the PDC magnitude did, and (ii) to weight properly different frequency bands according to the strength of the direct coupling. Consequently, we propose to define here a PDC based causality index measure, noted CI-PDC, by

$$CI_{mn}\text{-PDC} = \text{Im} \left( \sum_{f \in F} PDC_{mn}^*(f) PDC_{mn}(f + \delta_f) \right). \quad (16)$$

If the only contribution of the signal  $x_m$  into the signal  $x_n$  is due to a pure delay, the phase of  $D_{nm}(f)$  as well as the phase of PDC are linear, so that CI-PDC represents the slope of this phase, weighted by the magnitude of PDC.

### 2.5. Effect of deviation from linear model hypothesis

In some applications the model given in (10) is not the more realistic one and a non linear regression model (17) would be more suited

$$\begin{pmatrix} x_1(t) \\ \vdots \\ x_Q(t) \end{pmatrix} = \begin{pmatrix} g_1(x_1^d, \dots, x_Q^d, w_1)(t) \\ \vdots \\ g_Q(x_1^d, \dots, x_Q^d, w_Q)(t) \end{pmatrix}, \quad x_i^d(t) = (L^k x_i(t))_{k=1, \dots, d}, i = 1, \dots, Q \quad (17)$$

where  $g_i, i = 1, \dots, Q$ , are non linear functions. The efficiency of a linear model (10) to detect non linear incidence from channels  $m \in M_1 \subset \{1, \dots, Q\}$  to channel  $n$  (from  $x_m^d, m \in M_1$ , to  $x_n$ ) then depends a priori on the ability of a decomposition

sum  $g_n \left( \left( x_m^d \right)_{m \in M_{n,1}} \right) (t) + g_{n,2} \left( \left( x_m^d \right)_{m \in M_{n,2}}, w_n \right) (t)$  to approximate the function  $g_n(x_1^d, \dots, x_Q^d, w_n)(t)$  where

$M_{n,1} \cup M_{n,2} \subset \{1, \dots, Q\}, M_{n,1} \cap M_{n,2} = \emptyset$ ;  $g_{n,1}$  is a linear function and  $g_{n,2}$  is non linear. Only if the difference between

$g_n$  and  $g_{n,1} + g_{n,2}$  is not too important, we can expect that the indices described above remain relevant. Otherwise, in

presence of strong non linearities the  $g_{n,2}$  functions could be estimated by more sophisticated techniques based for exam-



ple on local linear approximations around reference points [6]. Nevertheless note that in this case the phase slope information could be less adapted, since it cannot capture phase relation between two different frequencies.

### 3. Experimental results

The different approaches were tested on models simulating practical situations and, for all of them, spectral estimation was based on AR modeling which can improve the estimator and reduce its variance as indicated in [20]. For each model, simulations were carried out 500 times on 1024-point signals (corresponding to 4 s duration with a sampling rate equal to 256 Hz). We calculated  $N$  frequency points regularly spaced, with  $N = 512$ , and the frequential step-size  $\delta_f$  was equal to 0.25 Hz. In our experiments, the AR coefficients and the order of the models were firstly estimated from the generated data by minimizing Akaike's information criterion (AIC) [1]. This was performed by using the functions `lsqr` and `aic` in MATLAB which, supposing Gaussian innovations, maximize a likelihood function through a least squares (LS) procedure [10] (chapter 16, section 16.4). Given these estimated parameters, we computed matrices  $H(f)$  and  $D(f)$  of Eqs. (7), (12) and (11) respectively by substitution of theoretical AR coefficients with the estimated ones. This procedure allows for obtaining CI-DCOH, CI-DTF and CI-PDC. Results are summarized in Tables 1 to 4, where the first value corresponds to the experimental mean of the indicator and the experimental standard deviation (sd) is in brackets.

#### 3.1. Linear models

We start by analyzing the behavior of our estimators on signals exhibiting bidirectional propagation flows (model 1). Then, we test them on a model (model 2) displaying direct and indirect connections.

##### 3.1.1. Model 1

For the first linear stochastic system, three signals were generated by the following equations

$$\begin{cases} x_1(t) = 0.95\sqrt{2}x_1(t-1) - 0.9025x_1(t-2) + w_1(t) \\ x_2(t) = -0.5x_1(t-1) - bx_3(t-3) + w_2(t) \\ x_3(t) = 0.8x_2(t-2) + w_3(t) \end{cases} \quad (18)$$

where  $w_j(t)$ ,  $j = 1, 2, 3$ , are independent white Gaussian noises with zero means and unit variances, the parameter  $b$  was introduced to consider two patterns of causal interactions with unidirectional ( $b = 0$ ; Fig. 1(a)) or bidirectional ( $b = 0.8$ ; Fig. 1(b)) relations between signals  $x_2$  and  $x_3$ . Means and standard deviations of PSI, CI-DCOH and CI-DTF were computed and shown in Table 1.

- *Results on PSI*

From Table 1, when there are only unidirectional (direct and/or indirect) information flows, *i.e.*  $b = 0$ ,  $\text{PSI}_{12}$ ,  $\text{PSI}_{23}$  and  $\text{PSI}_{13}$  gave positive values indicating that  $x_2$  is a delayed version of  $x_1$ , and  $x_3$  some delayed version of  $x_2$  and  $x_1$ . When there is a bidirectional information flow between  $x_2$  and  $x_3$  (*i.e.*  $b = 0.8$ ), PSI necessarily fails in detecting the flows due to its symmetric character ( $\text{PSI}_{32}$  is the opposite of  $\text{PSI}_{23}$ ). This result confirms that PSI is only able to point out

unidirectional flows.

- *Results on CI-DCOH*

In Table 1, considering the case  $b = 0$ , when there is no information flow, *i.e.* from  $x_2$  to  $x_1$ , or from  $x_3$  to  $x_1$ , or from  $x_3$  to  $x_2$ , the corresponding CI-DCOH remains close to zero. On the other hand, when unidirectional information flows exists, *i.e.* from  $x_1$  to  $x_2$ , or from  $x_1$  to  $x_3$ , or from  $x_2$  to  $x_3$ , the corresponding CI-DCOH largely increases. Considering the case  $b = 0.8$ , the same conclusions hold. Moreover, in this case of bidirectional flow between  $x_2$  and  $x_3$ , CI-DCOH is also able to determine this particular propagation, so that it appears as a relevant indicator to detect unidirectional and bidirectional relations.

- *Results on CI-DTF*

For the case  $b = 0$ , the very low values of  $CI_{21}$ -DTF,  $CI_{31}$ -DTF and  $CI_{32}$ -DTF are clearly justified as well as the great values of  $CI_{12}$ -DTF,  $CI_{13}$ -DTF and  $CI_{23}$ -DTF due to only unidirectional flows. For the case  $b = 0.8$ , all unidirectional and bidirectional flows are also properly detected. Therefore, CI-DTF behaves well in all situations and proves efficient in drawing the real propagation graphs.

In a second step, we compare the performance of CI-DCOH and CI-DTF from Table 1. On the one hand, whatever the value of  $b$ , the values of CI-DCOH are greater than those given by CI-DTF for the flow from  $x_2$  to  $x_3$ . On the other hand, in the bidirectional situation (*i.e.*  $b = 0.8$ ), the ratio  $CI_{32}$ -DTF/ $CI_{23}$ -DTF is closer to 3/2 corresponding to the ratio of the delays between signals  $x_2$  and  $x_3$ .

### 3.1.2. Model 2

For the second linear stochastic system we considered, the signal propagation situation was formalized as

$$\begin{cases} x_1(t) = 0.95\sqrt{2}x_1(t-1) - 0.9025x_1(t-2) + w_1(t) \\ x_2(t) = -0.5x_1(t-1) - 0.8x_3(t-3) + w_2(t) \\ x_3(t) = 0.8x_2(t-2) + cx_1(t-4) + w_3(t) \end{cases} \quad (19)$$

where  $w_j(t)$ ,  $j = 1, 2, 3$ , are independent white Gaussian noises with zero means and unit variances, and the parameter  $c$  was chosen to consider two patterns of interactions including indirect ( $c = 0$ ; Fig. 1(b)) and direct ( $c = 0.5$ ; Fig. 1(c)) relationships from signal  $x_1$  to signal  $x_3$ . In this system, a bidirectional flow was modeled between signals  $x_2$  and  $x_3$ . Means and standard deviations of CI-DCOH, CI-DTF and CI-PDC are calculated and presented in Table 2.

- *Results on CI-DCOH*

As already shown in Table 1, CI-DCOH allows for pointing out of unidirectional and bidirectional relations (see Table 2, either  $c = 0$  or  $c = 0.5$ ). On the other hand, when two different interactions exist from  $x_1$  to  $x_3$ , *i.e.* indirect ( $c = 0$ ) and direct ( $c = 0.5$ ,  $x_1$  connects to  $x_3$  via two distinct pathways) interactions,  $CI_{13}$ -DCOH reveals comparable values and, so, it becomes impossible to distinguish between direct and indirect interactions.

- *Results on CI-DTF*

As previously, we can conclude from Table 2 that CI-DTF succeeds in pointing out unidirectional and bidirectional relations but fails in distinguishing direct and indirect relations like CI-DCOH. Nevertheless, even if CI-DTF cannot reveal the delays between signals in the bidirectional case, one can at least infer the value of the delays' ratio between  $x_2$  and  $x_3$  (a 2-time delay from  $x_2$  to  $x_3$  and a 3-time delay from  $x_3$  to  $x_2$ ). As a matter of fact, the ratio  $CI_{32}\text{-DTF}/CI_{23}\text{-DTF}$  is always around 3/2 regardless if  $c = 0$  or  $c = 0.5$ , whereas the ratio  $CI_{32}\text{-DCOH}/CI_{23}\text{-DCOH}$  varies more (around 0.6 when  $c = 0$  and 1.0 when  $c = 0.5$ ).

- *Results on CI-PDC*

Like CI-DCOH and CI-DTF, from Table 2 CI-PDC succeeds in detecting unidirectional and bidirectional relations.

Moreover, when there is only indirect flow from  $x_1$  to  $x_3$  (for  $c = 0$ ),  $CI_{13}\text{-PDC}$  remains close to zero; and, when there is direct relation from  $x_1$  to  $x_3$  (for  $c = 0.5$ ),  $CI_{13}\text{-PDC}$  increases significantly. In this way, CI-PDC clearly contrasts with CI-DCOH and CI-DTF, since these two quantities always display a non negligible value when tested from signal 1 to signal 3, whatever the value of  $c$ . Therefore, CI-PDC resolves the existence of direct and indirect connections between pairs of signals by distinguishing these kinds of connections.

Finally, for the bidirectional relation between  $x_2$  and  $x_3$ , the ratios  $CI_{32}\text{-PDC}/CI_{23}\text{-PDC}$  are close to 3/2 regardless if  $c = 0$  or  $c = 0.5$  like CI-DTF. Furthermore, the value of  $CI_{23}\text{-PDC}$  (resp.  $CI_{32}\text{-PDC}$ ) is greater than the value of  $CI_{23}\text{-DTF}$  (resp.  $CI_{32}\text{-DTF}$ ), which appears more justified corresponding to some smoothing of the noise influence.

### 3.2. *Nonlinear models*

To test the robustness of our estimators to nonlinearity, we first tested a nonlinear model (model 3) where the coupling between signals is still linear. In a second step, the nonlinearity of the coupling is also taken into account (model 4).

#### 3.2.1. *Model 3*

The first nonlinear stochastic system we investigated was as follows:

$$\begin{cases} x_1(t) = 3.4x_1(t-1)(1-x_1^2(t-1))e^{-x_1^2(t-1)} + w_1(t) \\ x_2(t) = 3.4x_2(t-1)(1-x_2^2(t-1))e^{-x_2^2(t-1)} - 0.5x_1(t-1) - 0.8x_3(t-3) + w_2(t) \\ x_3(t) = 3.4x_3(t-1)(1-x_3^2(t-1))e^{-x_3^2(t-1)} + 0.8x_2(t-2) + cx_1(t-1) + w_3(t) \end{cases} \quad (20)$$

where  $w_j(t)$ ,  $j = 1, 2, 3$ , are independent white Gaussian noises with zero means and unit variances, and the parameter  $c$  was introduced to model direct or indirect interactions as in Eq. (19). Here we have  $g_2\left(\left(x_m^d\right)_{m \in \{1,2,3\}}, w_2\right)(t) = g_{2,1}\left(\left(x_m^d\right)_{m \in \{1,3\}}\right)(t) + g_{2,2}\left(\left(x_m^d\right)_{m=2}, w_2\right)(t)$ , and so we can expect to detect the influences from  $x_1$  and  $x_3$  to  $x_2$  with linear methods. Similarly, we can expect to detect the influences from  $x_1$  and  $x_2$  to  $x_3$  with lin-

ear methods according to  $g_3\left(\left(x_m^d\right)_{m \in \{1,2,3\}}, w_3\right)(t) = g_{3,1}\left(\left(x_m^d\right)_{m \in \{1,2\}}\right)(t) + g_{3,2}\left(\left(x_m^d\right)_{m=3}, w_3\right)(t)$ . Means and standard deviations of CI-DCOH, CI-DTF and CI-PDC are given in Table 3.

- *Results on CI-DCOH and CI-DTF*

Means and standard deviations of CI-DCOH and CI-DTF highlighted the ability of these two indices to put forward unidirectional and bidirectional interactions. As in the second linear model (see section 3.1.2, Eq. (19)), both CI-DCOH and CI-DTF could not differentiate between direct and indirect interactions from signal  $x_1$  to signal  $x_3$ .

Comparing CI-DCOH and CI-DTF, if we consider the relations between  $x_2$  and  $x_3$ , we first observe that CI-DTF displays greater values in the nonlinear model than in the linear one (model 2) unlike CI-DCOH. As in the linear case, this result is explained by the signals' characteristics. Secondly, in this bidirectional case, CI-DTF is still representative of the relative dependence that exists between  $x_2$  and  $x_3$ : the ratio  $CI_{32}\text{-DTF}/CI_{23}\text{-DTF}$  is around 3/2 regardless of the model (linear or nonlinear) and the pattern (indirect and direct interactions from  $x_1$  to  $x_3$ ).

- *Results on CI-PDC*

Results on CI-PDC reported in Table 3 lead to the same conclusions as those derived in the linear case (see section 3.1.2). CI-PDC acts as the most suitable and relevant indicator not only in detecting unidirectional and bidirectional relations but also in differentiating direct and indirect relations. For the bidirectional relation between  $x_2$  and  $x_3$ , the ratios  $CI_{32}\text{-PDC}/CI_{23}\text{-PDC}$  are also closer to 3/2 regardless of the value of  $c$  like CI-DTF. Moreover,  $CI_{23}\text{-PDC}$  (resp.  $CI_{32}\text{-PDC}$ ) is also greater than  $CI_{23}\text{-DTF}$  (resp.  $CI_{32}\text{-DTF}$ ) which is a worthwhile expected result.

### 3.2.2. Model 4

The second nonlinear stochastic system with nonlinear coupling was generated by the equations

$$\begin{cases} x_1(t) = 3.4x_1(t-1)\left(1-x_1^2(t-1)\right)e^{-x_1^2(t-1)} + w_1(t) \\ x_2(t) = 3.4x_2(t-1)\left(1-x_2^2(t-1)\right)e^{-x_2^2(t-1)} - 0.8x_1^2(t-3) - 0.8x_3(t-3) + w_2(t) \\ x_3(t) = 3.4x_2(t-1)\left(1-x_2^2(t-1)\right)e^{-x_2^2(t-1)} + 0.8x_2(t-2) + cx_1(t-1) + w_3(t) \end{cases} \quad (21)$$

where  $w_j(t)$ ,  $j=1,2,3$ , are independent white Gaussian noises with zero means and unit variances, and the parameter  $c$  was introduced to model direct or indirect interactions as in Eq. (19). Here we have  $g_2\left(\left(x_m^d\right)_{m \in \{1,2,3\}}, w_2\right)(t) = g_{2,1}\left(\left(x_m^d\right)_{m=3}\right)(t) + g_{2,2}\left(\left(x_m^d\right)_{m=1,2}, w_2\right)(t)$ , and we can expect to detect the influences from  $x_3$  to  $x_2$  with linear methods. Similarly for the third signal, we can expect to detect the influences from  $x_1$  to  $x_3$  with linear methods according to  $g_3\left(\left(x_m^d\right)_{m \in \{1,2,3\}}, w_3\right)(t) = g_{3,1}\left(\left(x_m^d\right)_{m=1}\right)(t) + g_{3,2}\left(\left(x_m^d\right)_{m=2}, w_3\right)(t)$  (according to the definition retained in section 2.5, all delayed versions of signal  $x_2$  are included in the nonlinear function  $g_{3,2}$ ). Note that, comparing with model 3, we introduced in model 4 a nonlinear coupling to test the influence of linearity versus nonlinearity of coupling. Means

and standard deviations of CI-DCOH, CI-DTF and CI-PDC are given in Table 4. Despite a global increase in the standard deviation, the mean values of the different indicators are of the same order of magnitude as those shown in Table 3. Considering CI-DCOH, when comparing signals two by two, we note that this indicator is affected by the nonlinear coupling to detect correctly the relations between  $x_1$  and  $x_2$ , as well as between  $x_1$  and  $x_3$ . On the other hand, the CI-DTF indicator allows detecting unidirectional and bidirectional relations despite the introduction of this nonlinear coupling and CI-PDC still performs well in differentiating direct and indirect relations.

#### 4. Discussion and conclusion

As shown in this study, the information flows among multivariable observations can display different patterns including unidirectional and/or bidirectional relations, direct and/or indirect relations. The original ordinary coherence based phase slope index only appears suitable to detect unidirectional flows when considering two time series. In this paper, we focus on information propagation between multi-site observations. The interest of the techniques we propose can be summarized as follows: (i) the introduction of directed coherence (DCOH) and directed transfer function (DTF) allows for dealing with unidirectional and bidirectional relations; (ii) moreover, the introduction of partial directed coherence (PDC) allows for distinguishing direct and indirect relations for unidirectional as well as bidirectional flow. In so far as we know, only amplitudes of DCOH, DTF and PDC have already been investigated to deal with the difficult issue of coupling between time series. In this contribution, both amplitudes and phases of these functions have been introduced to develop new causality indices that appear more relevant to flow propagation. Among the different techniques, the partial directed coherence function based approach has an advantage over the others since it takes into account only the direct contribution of a signal  $x_m$  on another signal  $x_n$  to compute the corresponding phase slope. It behaves well in distinguishing direct and indirect relations either for unidirectional or bidirectional flows. Now, if CI-PDC seems to be the best technique to differentiate all patterns in the proposed linear and nonlinear multivariate autoregressive models, real biological patterns may be more complex (EEG, ECG, EMG, etc.), which support the proposal of these different indicators. Moreover, according to EEG models found in the literature [7, 19], we can expect that in many practical cases the nonlinearities are sufficiently smooth, so that the indicators remain relevant. In the future, we plan to test them to characterize the underlying network organization of an epileptic seizure, in some difficult situation where time shifts between signals vary strongly in time. Clearly practical use of these indicators will imply the introduction of decision thresholds to reject the null hypothesis (no connectivity). Classically, as it is difficult to obtain theoretical distribution under independence, it will be necessary to obtain it empirically, for example using surrogate data. In such a situation, as in many other applications involving more than two or three channels, the computational cost of linear AR identification and phase analysis is highly reduced compared to the case of non linear analysis, which can then be only considered to solve ambiguous cases. Finally, despite the basic idea behind the indices developed in this work, which can be viewed as detecting linear phase slopes associated with pure delay, this phase linearity does not need

to be verified to expect interesting results: only a monotonic phase variation with a significant mean slope is required. It is important to note that generally, when using DCOH and DTF, the phase linearity is not verified, due to the intrinsic definition of such quantities. In the same manner, the PDC based index corresponds to linear phase only when there is a unique contribution (in terms of delay) of a first signal to a second. In a future work, we can also search for other choices of functions  $\theta$  and  $C_{mm}$  in (3), depending on the index property we want to emphasize. To conclude, it could be also interesting to extend phase analysis based on linear regression models to a higher order phase analysis based on polynomial regression models.

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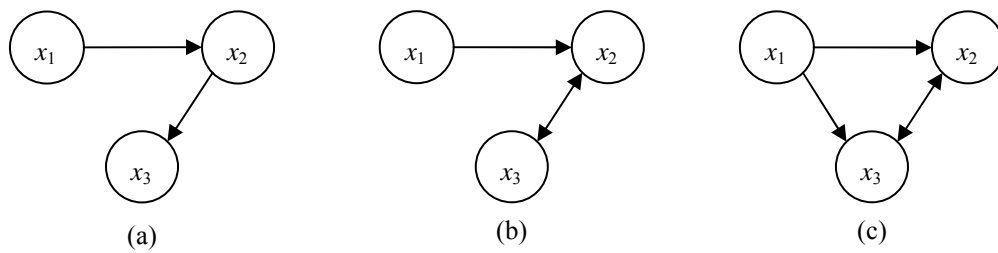
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**Fig. 1.** Three patterns of causal interactions. (a) Connection from signal  $x_1$  to signal  $x_3$  is indirect and mediated by signal  $x_2$ , and only unidirectional pathways exist. (b) Bidirectional flow exists between signals  $x_2$  and  $x_3$ . (c) Both direct and indirect connections exist from signal  $x_1$  to signal  $x_3$ , and bidirectional flow exists between signals  $x_2$  and  $x_3$ .



**Table 1.** Results on PSI, CI-DCOH and CI-DTF in Model 1 (Eq. (18))

		$b = 0$			$b = 0.8$				
		$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
<b>PSI</b>	$j = 1$	-	-0.9545 (0.0770)	-1.9548 (0.1348)	$j = 1$	-	-1.2295 (0.100)	-2.4176 (0.1614)	
	$j = 2$	0.9545 (0.0770)	-	-3.2289 (0.1241)	$j = 2$	1.2295 (0.1002)	-	-0.5720 (0.2248)	
	$j = 3$	1.9548 (0.1348)	3.2289 (0.1241)	-	$j = 3$	2.4176 (0.1614)	0.5720 (0.2248)	-	
<b>CI-DCOH</b>	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	
	$j = 1$	-	0.0103 (0.0019)	0.0117 (0.0023)	$j = 1$	-	0.0730 (0.0467)	0.0730 (0.0470)	
	$j = 2$	2.6657 (0.0804)	-	0.0840 (0.0509)	$j = 2$	3.0061 (0.1345)	-	2.5701 (0.2094)	
$j = 3$	3.6859 (0.1664)	3.8505 (0.1377)	-	$j = 3$	4.1662 (0.1837)	4.0941 (0.1889)	-		
<b>CI-DTF</b>	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	
	$j = 1$	-	0.0137 (0.0102)	0.0039 (0.0045)	$j = 1$	-	0.0308 (0.0235)	0.0352 (0.0262)	
	$j = 2$	2.7328 (0.0574)	-	0.0072 (0.0062)	$j = 2$	3.0772 (0.1031)	-	2.5662 (0.0933)	
$j = 3$	3.7738 (0.0932)	1.9548 (0.1056)	-	$j = 3$	4.2694 (0.1339)	1.7650 (0.0724)	-		

**Table 2.** Results on CI-DCOH, CI-DTF and CI-PDC in Model 2 (Eq. (19))

		$c = 0$			$c = 0.5$			
CI-DCOH	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
		$j = 1$	-	0.0730 (0.0467)	0.0730 (0.0470)	$j = 1$	-	0.1054 (0.0653)
	$j = 2$	3.0061 (0.1345)	-	2.5701 (0.2094)	$j = 2$	4.1472 (0.2722)	-	3.1384 (0.2443)
	$j = 3$	4.1662 (0.1837)	4.0941 (0.1889)	-	$j = 3$	4.4464 (0.2473)	3.1791 (0.2606)	-
CI-DTF	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
	$j = 1$	-	0.0308 (0.0235)	0.0352 (0.0262)	$j = 1$	-	0.0456 (0.0321)	0.0498 (0.0336)
	$j = 2$	3.0772 (0.1031)	-	2.5662 (0.0933)	$j = 2$	4.2191 (0.1785)	-	2.7103 (0.0910)
	$j = 3$	4.2694 (0.1339)	1.7650 (0.0724)	-	$j = 3$	4.5558 (0.2030)	1.8231 (0.0758)	-
CI-PDC	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
	$j = 1$	-	0.0065 (0.0063)	0.0043 (0.0036)	$j = 1$	-	0.0128 (0.0099)	0.0125 (0.0104)
	$j = 2$	0.9556 (0.0418)	-	3.6591 (0.0875)	$j = 2$	0.6210 (0.0459)	-	3.6596 (0.0932)
	$j = 3$	0.0094 (0.0092)	2.4443 (0.0622)	-	$j = 3$	2.4009 (0.0945)	2.4447 (0.0643)	-

**Table 3.** Results on CI-DCOH, CI-DTF and CI-PDC in Model 3 (Eq. (20))

		$c = 0$			$c = 0.5$			
	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
<b>CI-DCOH</b>	$j = 1$	-	0.0889 (0.0545)	0.0871 (0.0555)	$j = 1$	-	0.0835 (0.0483)	0.0847 (0.0567)
	$j = 2$	0.4756 (0.0839)	-	3.0785 (0.1747)	$j = 2$	1.3061 (0.1756)	-	2.9617 (0.1725)
	$j = 3$	0.9374 (0.1680)	2.7532 (0.1268)	-	$j = 3$	1.0996 (0.1523)	1.9809 (0.1096)	-
<b>CI-DTF</b>	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
	$j = 1$	-	0.0474 (0.0299)	0.0532 (0.0318)	$j = 1$	-	0.0467 (0.0286)	0.0525 (0.0301)
	$j = 2$	0.4451 (0.0743)	-	3.1826 (0.1152)	$j = 2$	1.2484 (0.1288)	-	3.0040 (0.1023)
	$j = 3$	0.8736 (0.1497)	2.2300 (0.0759)	-	$j = 3$	1.0376 (0.1256)	1.9990 (0.0712)	-
<b>CI-PDC</b>	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
	$j = 1$	-	0.0076 (0.0068)	0.0055 (0.0052)	$j = 1$	-	0.0076 (0.0067)	0.0052 (0.0045)
	$j = 2$	0.6384 (0.0627)	-	3.6723 (0.0869)	$j = 2$	0.5312 (0.0528)	-	3.6731 (0.0856)
	$j = 3$	0.0165 (0.0086)	2.4538 (0.0749)	-	$j = 3$	0.5335 (0.0534)	2.4518 (0.0623)	-

**Table 4.** Results on CI-DCOH, CI-DTF and CI-PDC in Model 4 (Eq. (21))

		$c = 0$			$c = 0.5$			
	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
<b>CI-DCOH</b>	$j = 1$	-	0.3382 (0.2086)	0.2418 (0.1701)	$j = 1$	-	0.3424 (0.2086)	0.2487 (0.1576)
	$j = 2$	0.2924 (0.2016)	-	1.7463 (0.2654)	$j = 2$	0.8793 (0.2315)	-	2.1051 (0.2704)
	$j = 3$	0.2189 (0.1598)	3.9366 (0.2559)	-	$j = 3$	0.4936 (0.1758)	3.6794 (0.2643)	-
<b>CI-DTF</b>	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
	$j = 1$	-	0.0562 (0.0325)	0.1132 (0.0698)	$j = 1$	-	0.0561 (0.0289)	0.1138 (0.0712)
	$j = 2$	0.2478 (0.1623)	-	4.0020 (0.3657)	$j = 2$	1.3283 (0.3085)	-	3.6388 (0.3526)
	$j = 3$	0.2432 (0.1546)	2.5270 (0.1745)	-	$j = 3$	0.6305 (0.1852)	2.2392 (0.1756)	-
<b>CI-PDC</b>	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$	$x_i \rightarrow x_j$	$i = 1$	$i = 2$	$i = 3$
	$j = 1$	-	0.0524 (0.0401)	0.0509 (0.0397)	$j = 1$	-	0.0521 (0.0402)	0.0512 (0.0396)
	$j = 2$	0.3235 (0.2164)	-	4.1335 (0.3325)	$j = 2$	0.3083 (0.2078)	-	4.1008 (0.3126)
	$j = 3$	0.0824 (0.0569)	2.5605 (0.0687)	-	$j = 3$	0.6793 (0.0852)	2.4555 (0.0745)	-